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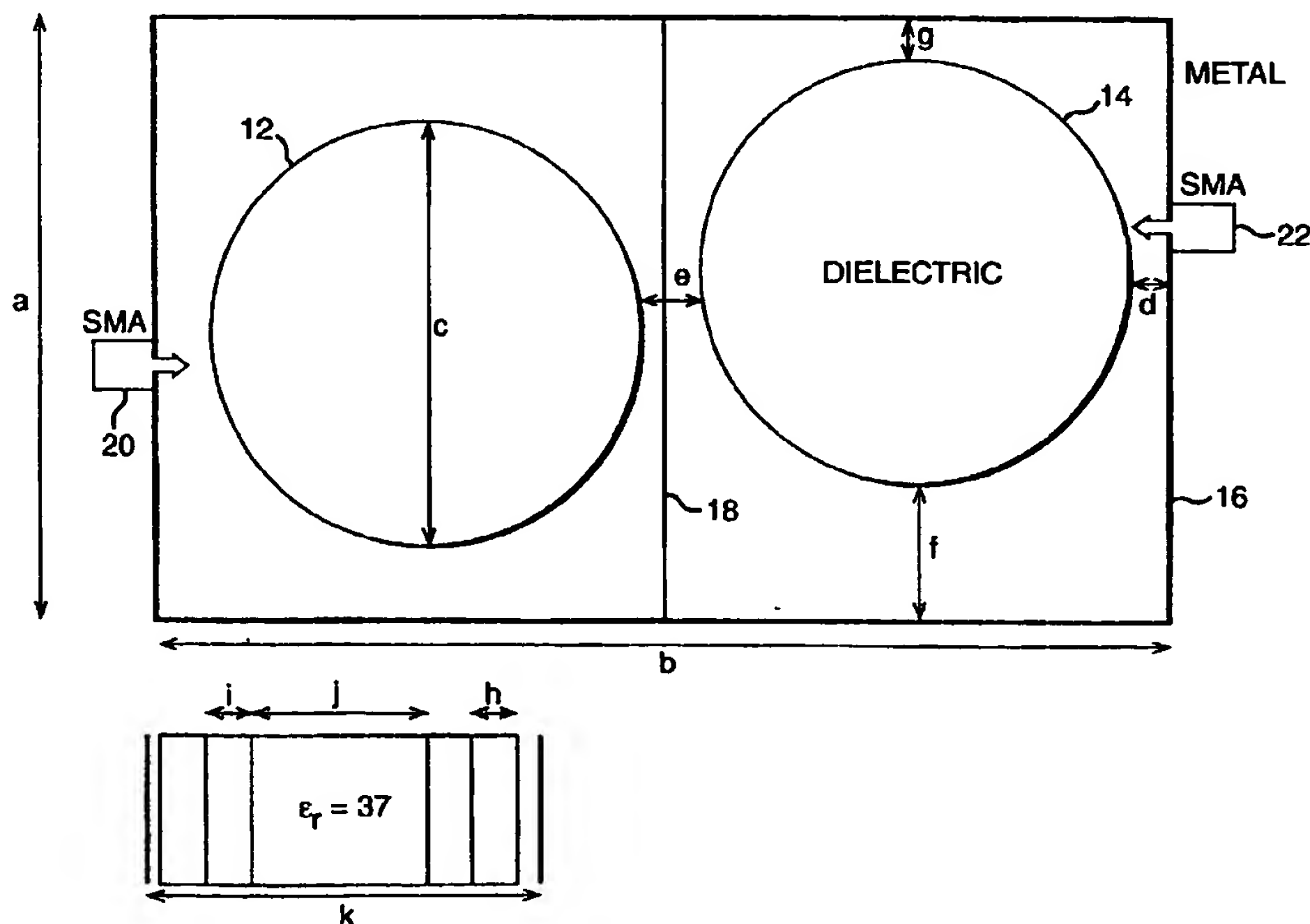
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(54) **Optimised resonator filter**

(57) The dimensions of a resonator filter comprising at least one puck (12, 14) in a metal cavity (16) are calculated by deriving the diameter c and thickness j of the puck, the spacing of the puck from the cavity walls

by a mode-matching technique, then optimised by applying electromagnetic simulation of a full filter response. Other dimensions of the puck may also be optimised. If two or more pucks are present in the cavity, the inter-puck spacing is also optimised.

FIG. 1



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Description

[0001] This invention relates to an optimised resonator filter, i.e. to a filter having dimensions optimised by a new method, and to a method for such dimension optimisation.

[0002] In wireless telecommunications at microwave frequencies, duplexers are used to transmit to and receive signals from an antenna. Currently available duplexers, which must have specified performance over a wide range of working temperatures, and required dimensions, carry material costs in the need to provide irises and tuning screws, and time costs in the need for a skilled person to tune the resonator before use.

[0003] It is an object of the invention to provide a resonator filter which does not need an iris or tuning or coupling screws but which still meets all technical requirements.

[0004] A mode-matching technique for the derivation of the response of a filter, using the dimensions of a resonator cavity and dielectric puck, has been published by D Kajfez and P Guillon, Dielectric Resonators, Oxford MS: Vector Fields, 1990.

[0005] Computer programs to derive a full filter response, based on electromagnetic simulation techniques, are commercially available.

[0006] It has now been realised that such programs can be used to optimise the parameters of a filter, and that the results can be used in filter design.

[0007] According to the invention a method of optimising the characteristics of a resonator filter comprising a dielectric puck in a conducting cavity characterised by deriving the diameter c and thickness j of the puck by a mode-matching technique; and optimising the diameter c and thickness j of the puck by electromagnetic simulation of a full filter response.

[0008] Also according to the invention a resonator filter comprising a puck of dielectric material within a conducting cavity, the diameter and thickness of the puck having been optimised by a method as set out above. Such a filter does not require tuning or coupling screws or an iris.

[0009] The invention will now be described by way of example with reference to the accompanying drawings in which:-

Figure 1 is a schematic drawing of a cavity resonator;

Figure 2 illustrates electromagnetic plots of the Figure 1 resonator;

Figure 3a is a calculated scattering parameter; and
Figure 3b is a measured scattering parameter.

[0010] In Figure 1, a cavity resonator 10 comprises two disc-shaped pucks 12, 14 of dielectric material within a metal cavity 16. The cavity had a dividing wall 18 between the pucks, and two SMA radio frequency connectors 20, 22.

[0011] The dimensions of the cavity 16 are a, b where $b = 2a$. Assume the two pucks 12, 14 are of identical dimensions. The puck diameter is c , the spacing of the puck 14 from the connector-bearing end wall is d , and from the two side walls of the cavity is f, g ; the spacing between the pucks 12, 14 is e .

[0012] Considering now further dimensions, j = length of the puck; h, i = the thickness of the puck support material; and k = total puck height, that is $k = h + j + i$.

[0013] The cavity 16 may be made of aluminium, and the pucks 12, 14 may be made of barium titanate, such as the material Ceramic D8300 (TM) supplied by Trans-tech of Adamstown, MD, USA, which has a dielectric constant of 37, a quality factor of 28,000 and an ultra-stable temperature coefficient of resonant frequencies.

[0014] Figure 2 illustrates the electromagnetic field plots of the resonator shown in Figure 1. The RF connectors 20, 22 are shown at different positions on the enclosure 16.

[0015] As is well known, for strong coupling between the pucks 12, 14, the dividing wall 18 can be removed; for weak coupling, the wall is left in place. For pucks with high permittivity, a wall may not be necessary.

[0016] Considering now the optimisation technique; in the first step, the mode-matching technique of Kajfez is applied to derive all of the dimensions a to k ; in the second step the derived parameters are loaded into an electromagnetic simulator program, such as the CST Microwave Studio 3D program which is based on a finite integration technique with perfect boundary approximation for three-dimensional electromagnetic simulation. The program is run to optimise the parameters, and the optimised parameters are then used to design a filter.

[0017] It has not previously been realised that such simulation programmes can be used to optimise the resonator parameters, with the result that tuning and coupling screws are no longer needed. The parameters are optimised by minimising the value of S_{11} , which is the reflection coefficient of the microwave in the band of the filter for each of the parameters a to k .

[0018] The technique may be applied to a single puck within a cavity. The technique may also be applied to a selected number of the dimensions shown in Figure 1; for a single puck, the most important dimensions are c, d, f, g and j . For two pucks in a cavity, the next most important dimension is the inter-puck spacing e .

[0019] For a Ceramic D8300 (TM) puck with a permittivity of 37 in an aluminium cavity, optimised dimensions are $a=53$ millimetres, $b=96$, $c=33$, $d=5$, $e=10$, $f=7$, $g=3$, $h=5$, $i=5$, $j=16.5$ and $k=36.5$. Typically the tolerances of the cavity wall dimensions are tens of micrometers.

[0020] In a further variation, the dimensions of a dividing wall 18 of the cavity are also optimised.

[0021] It has been found that a filter constructed with optimised parameters has a performance which is much more controllable and predictable than has previously been possible; the filter does not need tuning or coupling screws or an iris.

[0022] Figure 3 illustrates the calculated S-parameter magnitude in decibels for frequencies between 1.5 and 2×10^9 , for a 4 pole elliptic filter without tuning or coupling screws, and Figure 3b illustrates experimental values of the same parameter. In both figures the insertion loss is 0.19dB, return loss is 21dB, and out of band loss is 20dB.

[0023] An advantage of a filter without tuning or coupling screws or an iris is that the most expensive machined parts of the filter, which require expensive materials and tight tolerances, and the skill and therefore the time cost needed to tune a prior art filter, are no longer required.

[0024] Another advantage is that lower mid-band insertion losses are achievable than with a comparable filter having an iris and tuning and coupling screws, because conduction currents in the metallic cavity ends are eliminated.

[0025] A further advantage is that the physical size of the resonator can be reduced by a factor of 12 in comparison with an air filled resonator, by use of high dielectric constant and high quality factor dielectric material such as Ceramic D8300.

[0026] One application of a filter according to the invention is a duplexer in a microwave wireless communication system; such a duplexer is provided in the base stations of the GSM (Global System for Mobile Communications), when the front-end filtering requirement is 90dB attenuation in the stop-band; such a requirement can be met by a filter according to the invention.

5. A resonator filter comprising a puck (12 or 14) of dielectric material within a conducting cavity (16), characterised in that the diameter c and thickness j of the dielectric puck are optimised by a method according to Claim 1.
6. A resonator filter according to Claim 1 in which the thickness of the puck support material i , j and of the total puck thickness k are optimised by a method according to Claim 3.
7. A resonator filter according to Claim 5 or Claim 6 in which the spacing d , g , of the puck from the cavity wall is optimised by a method according to Claim 2.
8. A resonator filter comprising a plurality of pucks (12, 14) of dielectric material within a conducting cavity (16) characterised in that the dimensions of the puck, the dimensions of the cavity, and the spacing of the pucks from each other are optimised by a method according to Claim 4.
9. A resonator filter according to any one of Claims 5 to 8 which is without an iris or tuning or coupling screws.

Claims

1. A method of optimising the characteristics of a resonator filter comprising a dielectric puck in a conducting cavity characterised by deriving the diameter c and thickness j of the puck by a mode-matching technique and optimising the diameter c and thickness j of the puck by electromagnetic simulation of a full filter response.
2. A method according to Claim 1 further comprising deriving the spacing d , f , g , of the puck from the cavity wall by a mode-matching technique; and optimising the spacing of the puck from the cavity wall by electromagnetic simulation of a full filter response.
3. A method according to Claim 1 or Claim 2 further comprising deriving and optimising the thickness i , j of the puck support material and the total puck thickness k .
4. A method according to any one of Claims 1, 2 and 3 in which there are a plurality of pucks in the cavity further comprising optimising the separation e of the pucks from each other.

FIG. 1

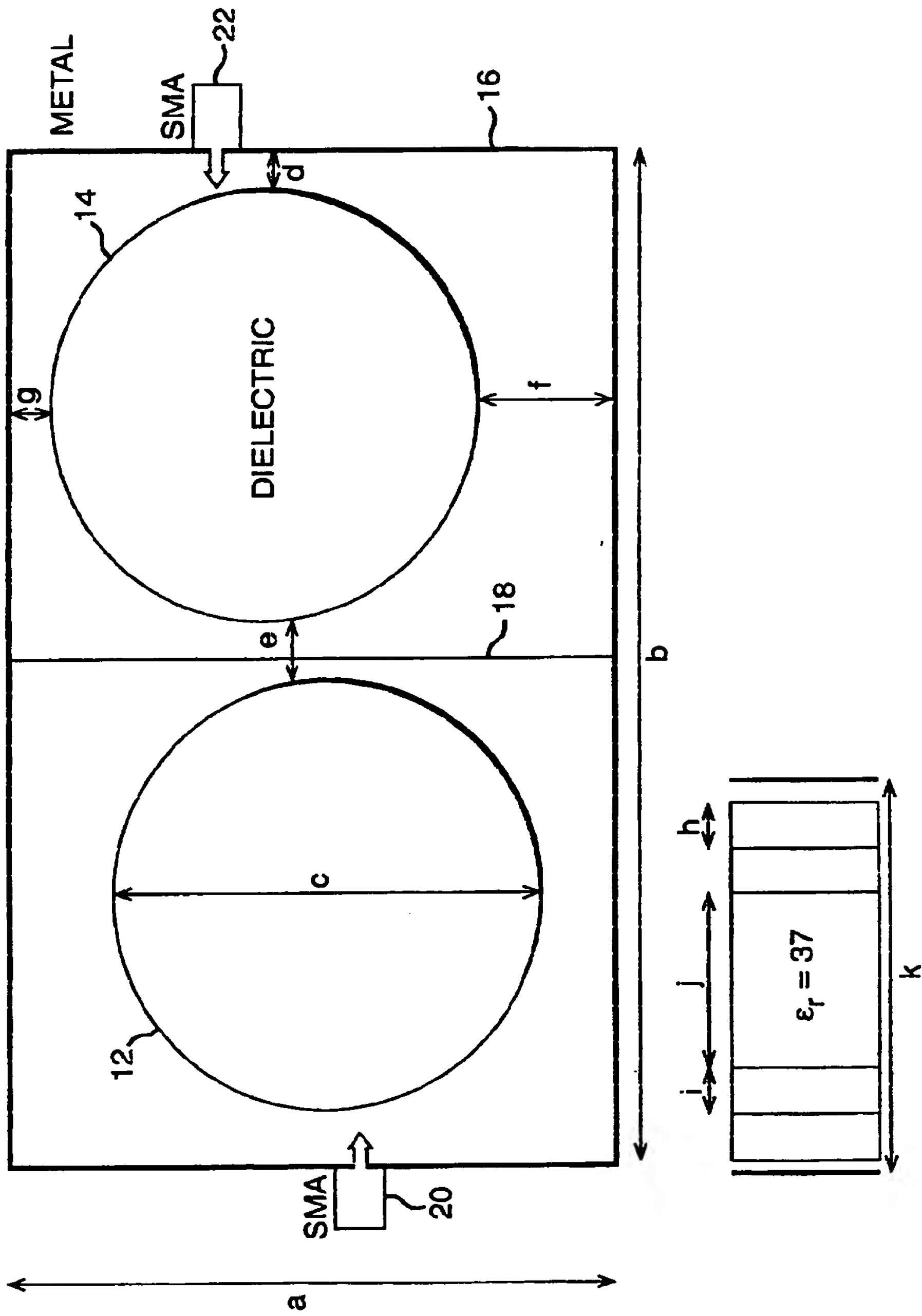


FIG. 2

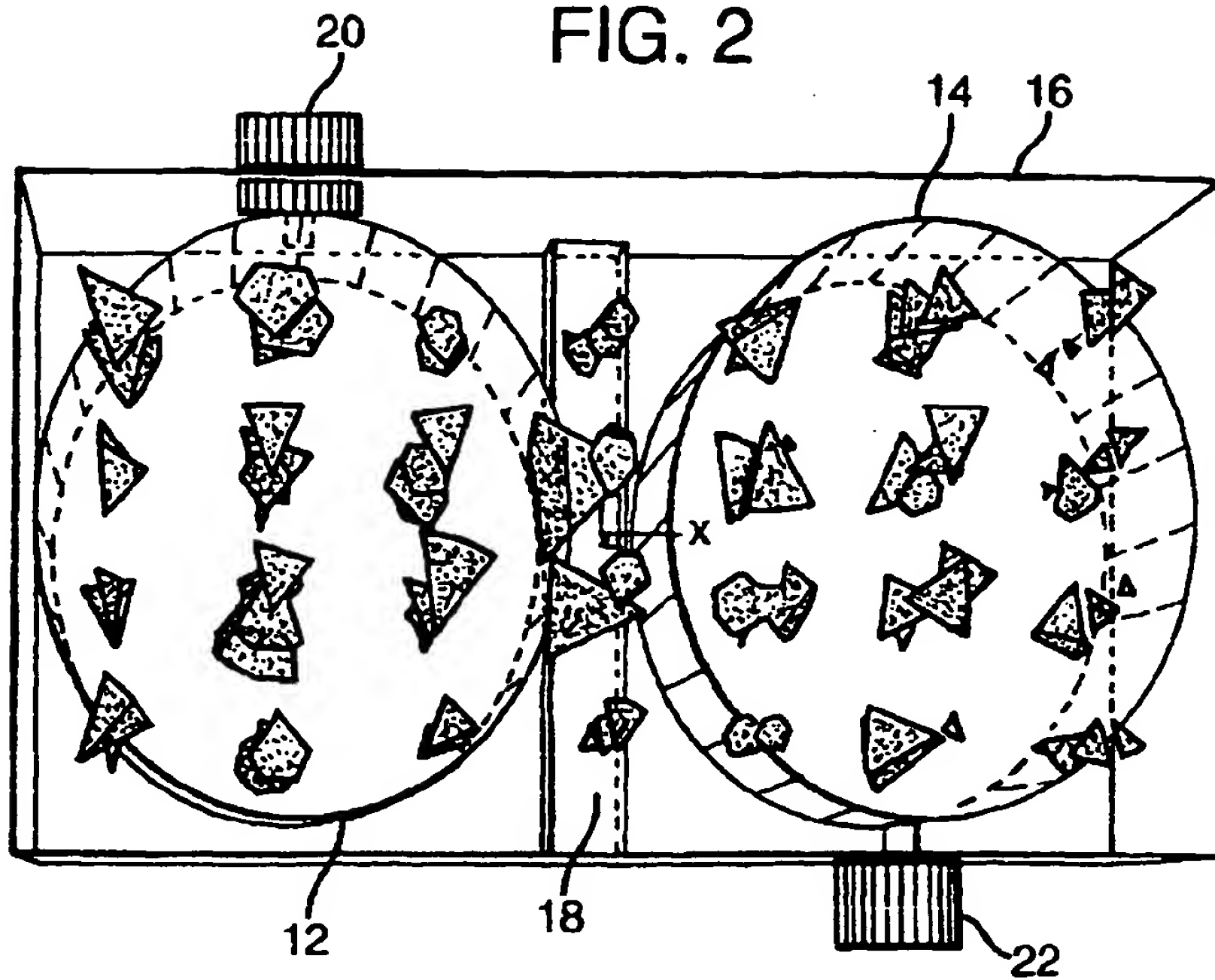
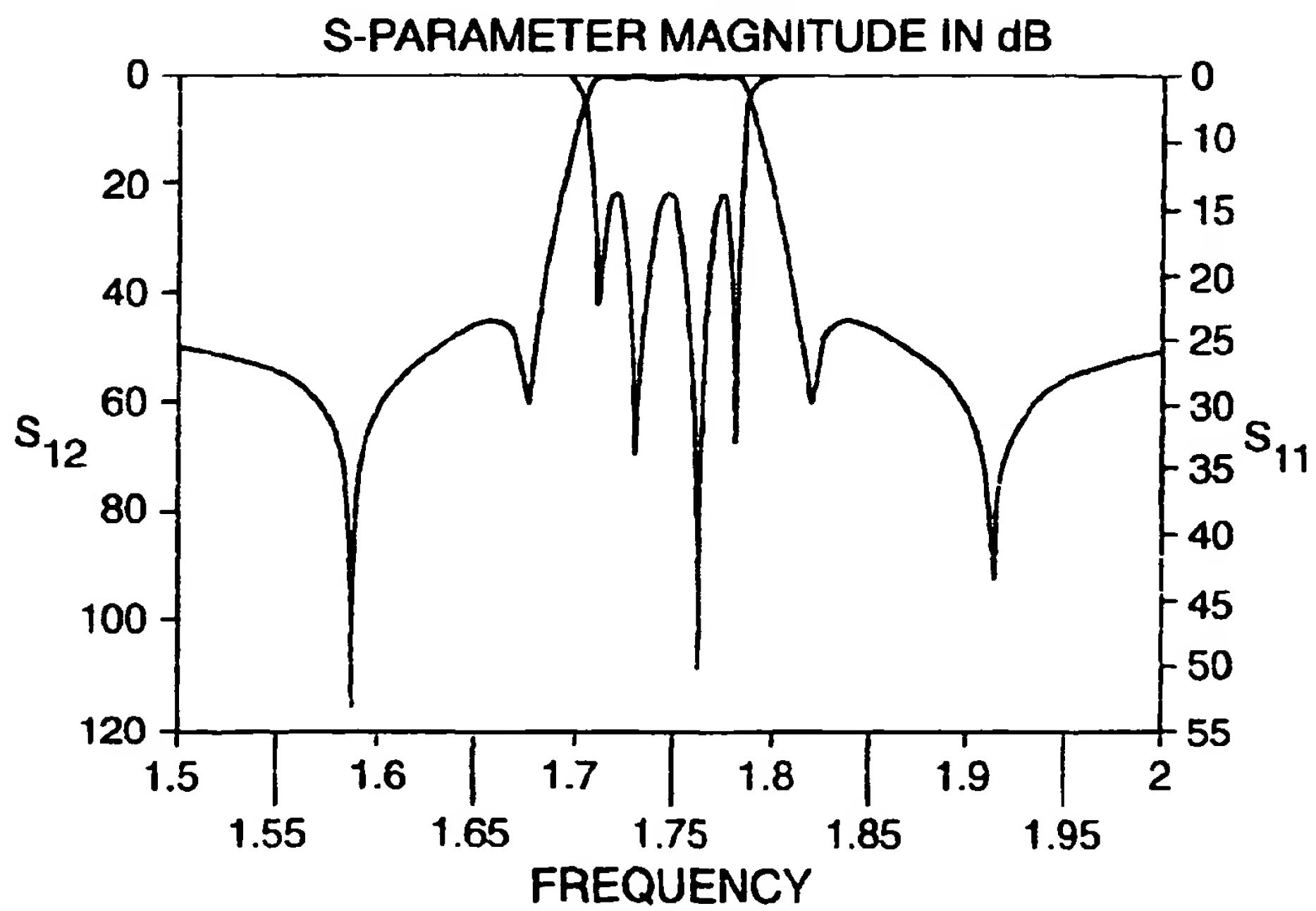
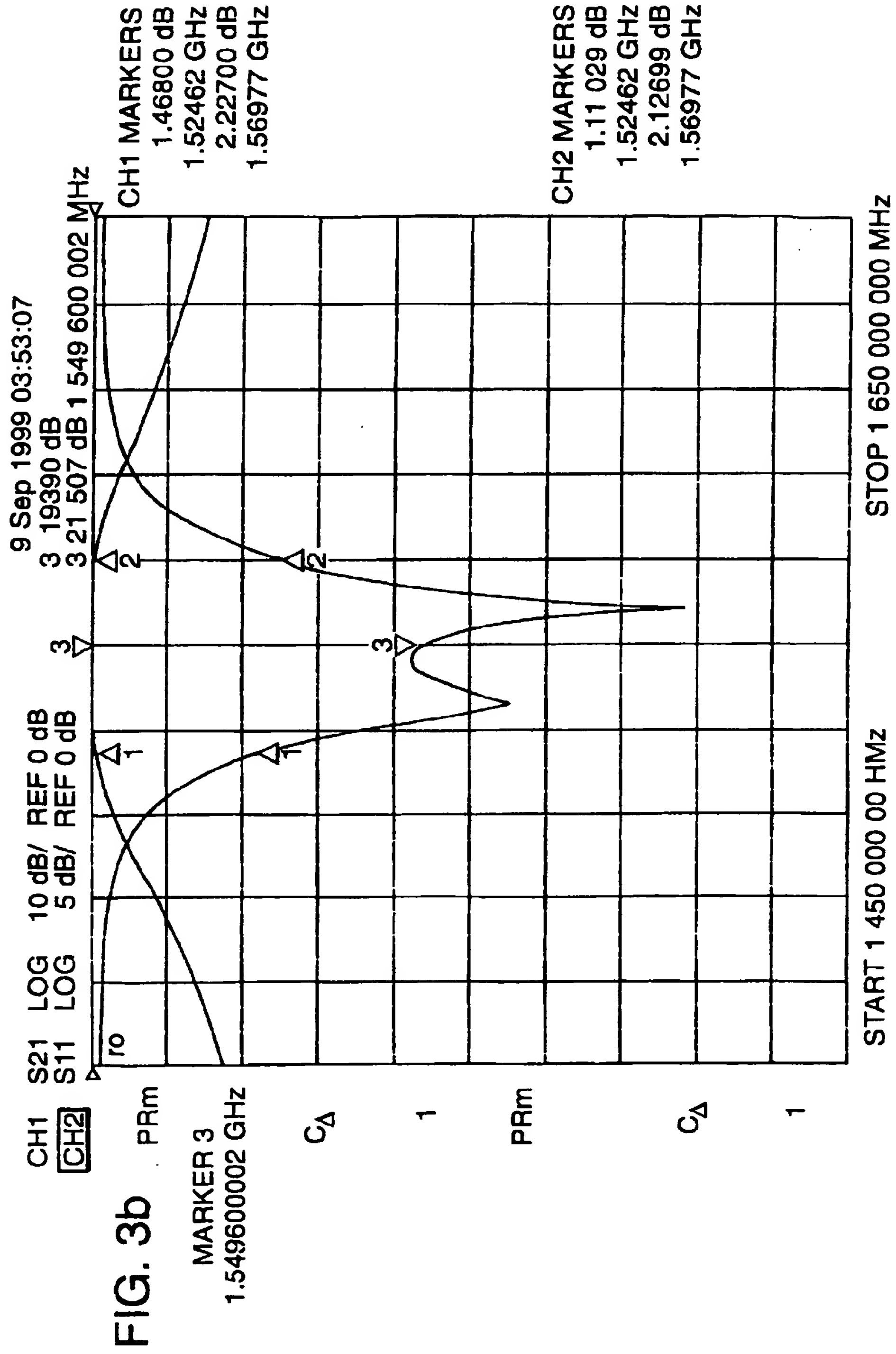


FIG. 3a







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EUROPEAN SEARCH REPORT

Application Number
EP 99 30 8191

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (InLCI.7)
A	<p>CHI WANG ET AL: "MIXED MODES CYLINDRICAL PLANAR DIELECTRIC RESONATOR FILTERS WITH RECTANGULAR ENCLOSURE"</p> <p>IEEE TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES,US,IEEE INC. NEW YORK, vol. 43, no. 12, PART 02, 1 December 1995 (1995-12-01), pages 2817-2823, XP000549431</p> <p>ISSN: 0018-9480</p> <p>* page 2819, left-hand column, line 25 - page 2821, left-hand column, line 2; figures 1,5 *</p>	1,5	<p>H01P1/208</p> <p>H01P7/10</p>
A	<p>---</p> <p>COUSTY J P ET AL: "FINITE ELEMENTS FOR MICROWAVE DEVICE SIMULATION: APPLICATION TO MICROWAVE DIELECTRIC RESONATOR FILTERS"</p> <p>IEEE TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES,US,IEEE INC. NEW YORK, vol. 40, no. 5, 1 May 1992 (1992-05-01), pages 925-932, XP000271379</p> <p>ISSN: 0018-9480</p> <p>* page 925, left-hand column, line 10 - line 20 *</p> <p>* page 925, right-hand column, line 7 - line 19; figures 4,12,15 *</p> <p>-----</p>	1	<p>TECHNICAL FIELDS SEARCHED (Int.Cl.7)</p> <p>H01P</p>
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 16 March 2000	Examiner Den Otter, A
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone</p> <p>Y : particularly relevant if combined with another document of the same category</p> <p>A : technological background</p> <p>O : non-written disclosure</p> <p>P : intermediate document</p> <p>T : theory or principle underlying the invention</p> <p>E : earlier patent document, but published on, or after the filing date</p> <p>D : document cited in the application</p> <p>L : document cited for other reasons</p> <p>-----</p> <p>& : member of the same patent family, corresponding document</p>			

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